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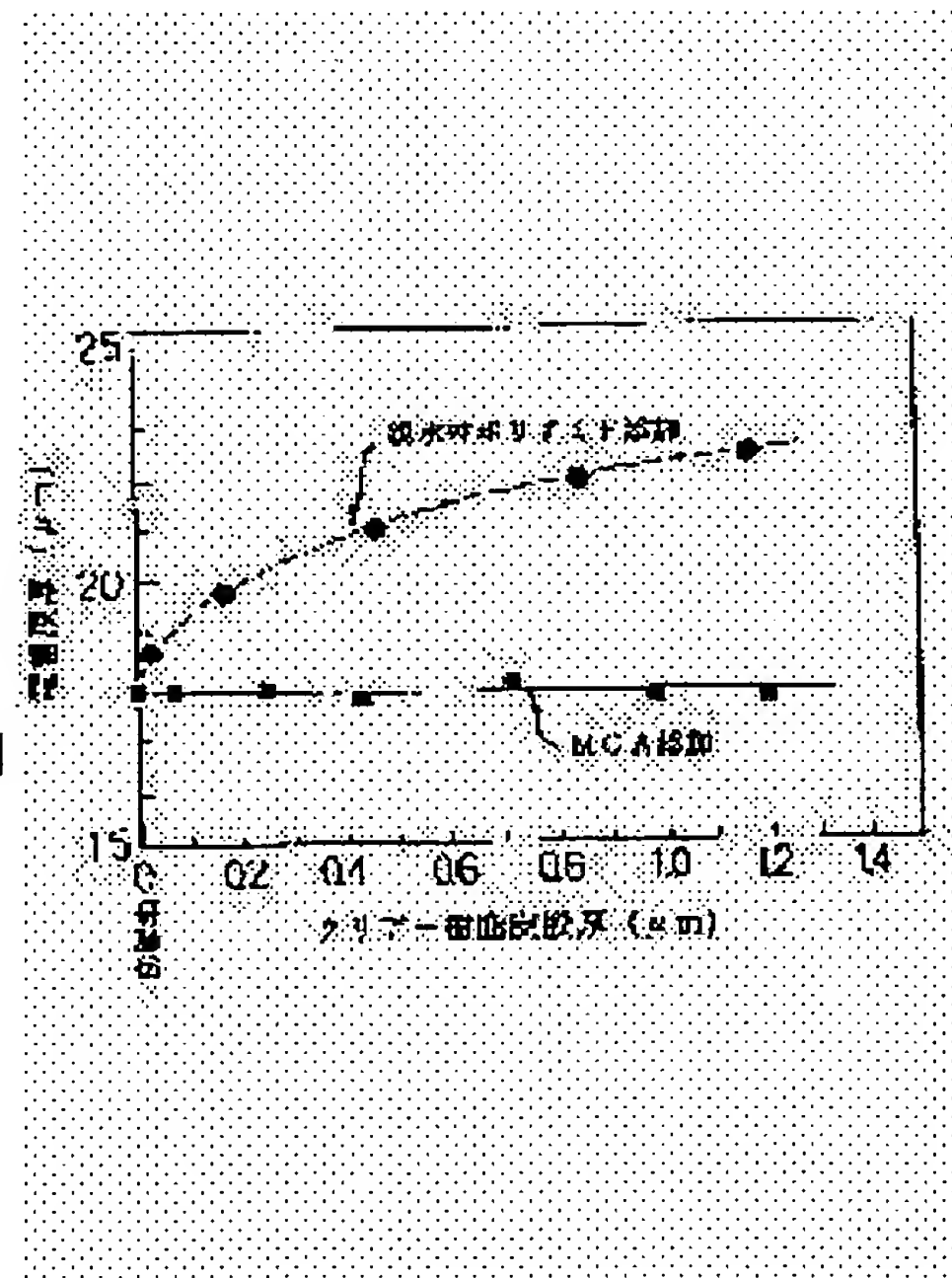
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## (54) SURFACE TREATED STEEL PANEL FOR CAR

(57)Abstract:

PURPOSE: To satisfy all of various properties (corrosion resistance, press moldability, spot weldability, cation electrodeposition painting properties, low temp. chipping resistance, sharpness after painting) required on the inner and outer surfaces of an exterior steel panel for a car in an org. composite surface treated steel panel wherein a chromate film and an org. resin film are provided on a zinc or zinc alloy (e.g. Zn-Ni, Zn-Fe) plated steel panel.

CONSTITUTION: A bright steel panel of which the surface roughness Ra is  $0.3\mu\text{m}$  or less on at least a single surface is used as a base material and the uppermost layer on the steel panel is composed of a crosslinked epoxy resin film containing 0.1-20wt.% of a melamine/cyanuric acid adduct and 1-20wt.% of polyolefin wax and having a film thickness of  $0.1\text{--}2.0\mu\text{m}$ . Silica is added to a chromate film containing 20-200mg/m<sup>2</sup> of metal Cr in such an amt. that a SiO<sub>2</sub>/Cr wt. ratio becomes 0.05-4.0 and/or 5-40wt.% of SiO<sub>2</sub> is added to the org. resin film.



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ABSTRACT:

PURPOSE: To satisfy all of various properties (corrosion resistance, press moldability, spot weldability, cation electrodeposition painting properties, low temp. chipping resistance, sharpness after painting) required on the inner and outer surfaces of an exterior steel panel for a car in an org. composite surface treated steel panel wherein a chromate film and an org. resin film are provided on a zinc or zinc alloy (e.g. Zn-Ni, Zn-Fe) plated steel panel.

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CLAIMS

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[Claim(s)]

[Claim 1] The one side side of a steel plate is 0.3 at Ra at least. It has the surface roughness below mum. It is 20 - 200 mg/m2 to the order from a lower layer on this front face by \*\* zinc or the zinc alloy plating layer, and \*\* metal Cr conversion. Chromate film, \*\* Consist of bridge formation epoxy system resin containing 0.1 - 20% of the weight of a melamine cyanuric acid addition product, and 1 - 20% of the weight of a polyolefine wax. Thickness 0.1-2.0 It has the organic resin coat of mum and a chromate film is a silica at a SiO2/Cr weight ratio further 0.05-4.0 [ whether it contains in the becoming amount, and ] And/or, the surface treated steel sheet for automobiles characterized by an organic resin coat containing a silica in 5 - 40% of the weight of SiO2 amount.

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[Translation done.]

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DETAILED DESCRIPTION

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[Detailed Description of the Invention]

[0001]

[Industrial Application] The outstanding cation electropainting nature is shown, the image clarity after paint is improved remarkably, and this invention relates to the surface treated steel sheet for automobiles with other good properties moreover required of steel plates for automobiles, such as corrosion resistance, low-temperature-proof chipping nature, spot welding nature, and press-forming nature.

[0002]

[Description of the Prior Art] The demand for the rust-proofing engine performance of an automobile car body is increasing severity for the year later on in recent years, and various surface treated steel sheets have been developed that this demand should be coped with. They are a galvanization or zinc alloy plating (an example, Zn-nickel, or Zn-Fe alloy plating) as part [ especially as opposed to / recently / the sheathing external surface of an automobile ] of a rust-proofing engine-performance strengthening measure. A steel plate is used as a base material and they are chromate treatment and a clear coating to this. (an example, epoxy system plastic paint containing a cross linking agent) Application of an organic compound surface treated steel sheet which gave thin organic resin covering to depend is advanced quickly.

[0003] However, since the conductivity of the upper organic resin coat was bad, even if it used the conventional organic compound surface treated steel sheet as the thin film, cation electropainting nature was not enough [ the surface treated steel sheet ]. Since also developing the demand to an automobile appearance increasingly together with the rust-proofing engine performance from now on was expected, the improvement of the electropainting nature which influences an appearance had become pressing need.

[0004] Forming the upper organic resin coat in JP,3-32638,B from the epoxy system resin containing hydrophilic polyamide resin as a remedy of the electropainting nature of an organic compound surface treated steel sheet is proposed. Although this surface treated steel sheet was equipped with the satisfying engine performance when the cation electropainting nature which surely was conventionally excellent compared with elegance was shown and was considered as an object for automatic in-the-car plates, when it uses it as an object for shell plates, it has the following troubles, and had to say that it was unsuitable as an object for automobile sheathing.

[0005] That is, if cation electropainting is given to this organic compound surface treated steel sheet, compared with the case where cation electropainting of the zinc system plating steel plate used as a base material of this surface treated steel sheet is carried out under the same conditions with nakedness, about 1-8 micrometers of electropainting thickness will become thick. For this reason, when it uses as a shell plate for automobiles, by the part by which the organic resin coat and the chromate film are shaved off like the press crack care-and-cleaning section, from that perimeter, electropainting thickness becomes thin and a paint appearance falls remarkably.

[0006] Apart from this, the trouble that the conventional organic compound surface treated steel sheet did not have enough low-temperature-proof chipping nature was also pointed out. Since the big residual



stress which produced the plating coat of a zinc system at the time of plating although the anti-corrosiveness of an organic compound surface treated steel sheet was mainly secured by the zinc or the zinc alloy plating coat of the lowest layer has been held, it is a low-temperature chipping. (phenomenon in which a plating layer exfoliates from an interface with a steel plate by the impact of a stone shuttlecock etc. in cold districts, such as Europe and North America) There was an inclination to be easy to be generated. Prevention of the low-temperature chipping which the corrosion resistance of an automobile is degraded remarkably and leads to aggravation of a life or an appearance for the surface treated steel sheet for automobile sheathing is important.

[0007] As a measure for this problem, it is the effective elasticity as shock absorbing material to a zinc system plating front face in JP,46-78832,A. (55 degrees C or less of glass transition points) Forming a resin coat is proposed. However, since corrosion resistance is low compared with bridge formation epoxy system resin etc., it becomes inadequate corrosion-resistant improving [ which is the key objective of a surface treated steel sheet ] elasticity resin. Furthermore, the problem of the poor appearance by thick-film-izing of electropainting as well as the above could not be escaped.

[0008] The important element which influences the appearance of an automobile is the image clarity after paint. The technique which rolls out a steel plate with the roll which performed laser processing as a means which raises the image clarity after paint, and forms a dull pattern from the former is known. s (an example, JP,62-168602,A, etc.) . Securing the flatness of a steel plate to some extent, this technique is made dull, in order to give oil holdout required for the lubrication at the time of press forming. In spite of having thought that the so-called dull bright steel sheet which is not was ideal for the image clarity after paint, Dahl who there is no oil holdout, and has irregularity in a steel plate front face in a bright steel sheet since press forming is impossible had to be formed.

[0009]

[Problem(s) to be Solved by the Invention] The purpose of this invention is offering the organic compound surface treated steel sheet for automobiles which filled all the engine performance required of an inside [ of an automobile sheathing material ], and external surface side.

[0010] The concrete purpose of this invention is offering the organic compound surface treated steel sheet for automobiles remarkably improved also about cation electropainting nature, low-temperature-proof chipping nature, and the image clarity after paint as well as having the outstanding corrosion resistance and press-forming nature, and spot welding nature.

[0011]

[Means for Solving the Problem] this invention persons are  $Ra \leq 0.3$  which is a base material ideal for an improvement of image clarity. Steel plate of mum (the so-called bright steel sheet) Press forming was possible by considering as a base material and forming the organic resin coat excellent in lubricity in the front face, and this invention was reached, as a result of repeating examination in order to obtain the organic compound surface treated steel sheet which fills various kinds of above-mentioned engine performance.

[0012] For this invention, the one side side of a steel plate is 0.3 at Ra at least here. It has the surface roughness below mum. It is 20 - 200 mg/m<sup>2</sup> to the order from a lower layer on this front face by \*\* zinc or the zinc alloy plating layer, and \*\* metal Cr conversion. Chromate film, \*\* Consist of bridge formation epoxy system resin containing 0.1 - 20% of the weight of a melamine cyanuric acid addition product, and 1 - 20% of the weight of a polyolefine wax. Thickness 0.1-2.0 It has the organic resin coat of mum and a chromate film is a silica at a SiO<sub>2</sub>/Cr weight ratio further 0.05-4.0 [ whether it contains in the becoming amount, and ] And/or, let the surface treated steel sheet for automobiles characterized by an organic resin coat containing a silica in 5 - 40% of the weight of SiO<sub>2</sub> amount be a summary.

[0013] The main descriptions of the organic compound surface treated steel sheet of this invention are degrees. (a) - (e) It is.

(a) Adopt a bright steel sheet as a base material steel plate aiming at an ultimate improvement of the image clarity after paint.

(b) the zinc system plating layer of a substrate, and a middle chromate film -- in addition, use the resin coat of the maximum surface as a precise hard bridge formation epoxy resin coat, and improve corrosion

resistance.

(c) Melamine cyanuric acid addition product which was excellent in lubricity in this resin coat (the following, MCA, and brief sketch) A polyolefine wax is added and advanced sliding nature is given to a coat. Consequently, even if a bright steel sheet is a base material, press forming becomes possible easily.

(d) According to the effectiveness of MCA blended into the resin coat, electropainting nature is also improved remarkably, without reducing corrosion resistance and spot welding nature.

(e) About the problem of the low-temperature chipping of a zinc system plating layer, blend a silica with both a chromate film, and resin both [ one side or ], and improve low-temperature-proof chipping nature.

[0014] As the above synthetic result, cation electropainting nature and the image clarity after paint are improved remarkably, and the organic compound surface treated steel sheet with which it can be satisfied of various kinds of engine performance required of the inside and external surface of the steel plate for automobiles, such as corrosion resistance, low-temperature-proof chipping nature, spot welding nature, and press-forming nature, about all is obtained.

[0015]

[Function] The reason for having adopted the above-mentioned configuration in the organic compound surface treated steel sheet of this invention is explained below with the operation.

[0016] (1) The surface roughness which is an ideal ingredient at the image clarity reservation after base material steel plate paint is  $Ra \leq 0.3$ . Steel plate of mum (bright steel sheet) It applies. Since there is no oil holdout and press forming was not completed conventionally, although a bright steel sheet is unsuitable as a base material steel plate, in this invention, it became applicable [ a bright steel sheet ] by giving advanced lubricity to the upper organic resin coat. The surface roughness of a steel plate is 0.3 at  $Ra$ . If mum is exceeded, the improvement effect of the image clarity after paint will become indefinite.

[0017] For image clarity, although only one side should have the above-mentioned surface roughness since it is the engine performance required of an external surface side, both sides are  $Ra \leq 0.3$  by the convenience of a production process. You may be the bright steel sheet of mum. although effectiveness is enough demonstrated only on external-surface side one side since press nature also improves sharply by improving the sliding nature by the side of a dice side that multilayer surface treatment covering which is explained below and which consists of a plating + chromate film + organic resin coat should just be fundamentally formed in external surface side one side, it is required of an inside side -- -proof -- since hole vacancy nature etc. is improved, it is also applicable to both sides.

[0018] (2) The substrate plating used as the lowest layer of substrate plating organic compound surface treatment is zinc or zinc alloy plating excellent in sacrifice corrosion prevention ability because of corrosion-resistant reservation. (henceforth zinc system plating) It considers as a coat. That is, as a base material steel plate of the surface treated steel sheet of this invention, the zinc system plating steel plate with which zinc system plating was performed is used. The amount of superintendent officers of this zinc system plating is 10 g/m<sup>2</sup> per one side from the purpose which raises external surface-proof \*\*\*\* although chosen according to corrosion resistance demand level. Considering as the above is desirable. Since press-forming nature will fall if there are too many amounts of superintendent officers, as for an upper limit, considering as about two 60 g/m is desirable.

[0019] Especially the class of zinc alloy plating is not limited, but may apply any of a Zn-nickel alloy plating, a Zn-Fe alloy plating, Zn-aluminum plating, or the well-known zinc system alloy plating that added Co, Ti, etc. further. Especially the approach of zinc system plating is not restricted, either. Although electroplating is desirable since there may be comparatively few amounts of superintendent officers, hot dipping and alloying hot dip zincing are sufficient. Moreover, a zinc system plating coat may be a double layer plating coat more than two-layer.

[0020] (3) Prepare a chromate film on a chromate film zinc system plating layer. A chromate film has the operation which improves further the corrosion resistance of the surface treated steel sheet which uses a zinc system plating steel plate as a base material. Moreover, if a chromate film is made to contain a silica, the operation which raises low-temperature-proof chipping nature will also be demonstrated.



Although both a spreading mold a reaction type and an electrolytic type are possible, the spreading mold chromate film excellent in especially corrosion resistance of the formation approach of a chromate film is desirable.

[0021] Into a chromate film, other additives added by the chromate film from the former other than the silica which can be added to arbitration can also be blended. As an example of this additive, there are a silane coupling agent, a rust preventive pigment, a phosphoric acid, a hydrofluoric acid, etc.

[0022] The coating weight of a chromate film is metal Cr conversion, and is 20 - 200 mg/m<sup>2</sup>. It carries out. 20 In less than two mg/m, neither the corrosion resistance of level required for automobile sheathing nor low-temperature-proof chipping nature can be secured, but coating weight is 200 mg/m<sup>2</sup>. If it exceeds, when press-forming nature and weldability will deteriorate, Cr elution volume at the time of cleaning and chemical conversion before paint increases. the desirable coating weight of a chromate film -- 20 - 150 mg/m<sup>2</sup> it is .

[0023] (4) The organic resin coat on an organic resin coat chromate film (clear coat) also achieves the operation which secures adhesion with an electrodeposited paint film, and the operation as a lubrication coat which gives sliding nature at the time of press forming at the same time it functions as a barrier layer which prevents a staining substance from preventing that Cr is eluted from a lower layer chromate film at the time of cleaning and chemical conversion of a surface treated steel sheet, and invading from the exterior. In this invention, it is precise and the bridge formation resin coat which uses epoxy system resin excellent in corrosion resistance as a principal component is used.

[0024] As epoxy system resin, various modified epoxy resins, such as a carboxyl group in a drying-oil fatty acid, epoxy ester resin which made it react, and an urethane modified epoxy resin obtained by making it react with isocyanate, can also use the epoxy group and hydroxyl in these epoxy resins for the glycidyl ether mold epoxy resin of arbitration, such as the bisphenol A system, a bisphenol F system, a novolak mold, and bromination epoxy, and a list. Furthermore, dihydric phenol (an example, resorcinol, and/or bisphenols) The resin named the polyhydroxy polyether resin which is made to carry out a polycondensation to the epihalohydrin of an equimolecular amount mostly under existence of an alkali catalyst, and is obtained generically is also contained in the epoxy system resin of this invention.

[0025] It is other resin if little to this epoxy system resin. (an example, acrylic resin, polyester resin, an alkyd resin, polyvinyl butyral resin, various water soluble resin) You may blend.

[0026] In order to carry out eburnation of the resin coat and to improve corrosion resistance, epoxy system resin is made to construct a bridge during stoving of a paint film by the cross linking agent, and it considers as a bridge formation resin coat. As a cross linking agent, phenol resin and amino resin well-known as a curing agent for epoxy resins, a polyamide, an amino polyamide, an amine, block isocyanate, an acid anhydride, etc. can be used. The addition of a cross linking agent is chosen so that the flexibility of the epoxy system resin coat which constructed the bridge may not be lost too much.

[0027] MCA and a polyolefine wax are made to contain in this bridge formation epoxy system resin coat in this invention. A silica may be made to contain further in order to aim at the improvement of low-temperature-proof chipping nature. Other arbitration addition components can also be made to contain in an epoxy system resin coat. For example, a silane coupling agent, inorganic fillers other than a silica s (an example, various silicate minerals, an alumina, calcium carbonate, etc.) Chromium metal acid chloride system rust preventive pigment (an example, a barium chromate, or strontium) One sort or two sorts or more can be added in the range which does not have a bad influence on the engine performance of an organic resin coat.

[0028] Moreover, for the purpose of giving epicritic [ of a front flesh side ], an organic resin coat is made to contain organic, an inorganic color pigment, or a color, and a coat may be colored. for example, case where organic compound surface treatment of this invention is performed only to one side of a steel plate (when carrying out surface treatment only of the external surface side for an example and automobile sheathing) \*\*\*\* -- by coloring an organic resin coat, discernment of a front flesh side becomes quite obvious, and the activity by the user becomes easy.

[0029] Thickness of an organic resin coat 0.1-2.0 It is referred to as mum. Thickness is 0.1. The operation effectiveness of the organic resin coat mentioned above is not fully acquired under by mum.



Thickness is 2.0. When mum is exceeded, the insulation of this coat becomes large, spot welding nature falls, and there is a possibility of causing damage and energization impossible of the chip at the time of welding.

[0030] If an organic resin coat needs to be formed, it will dilute epoxy system resin with a suitable organic solvent, and it prepares resin liquid. In this resin liquid A cross linking agent, MCA, and a polyolefine wax, If required, they are other addition components. s (an example, a silica sol, silane coupling agent, etc.) Nonvolatile matter (all components other than a solvent) Add, and it is made to dissolve thru/or distribute so that it may become predetermined loadings to sum total weight, and carries out by applying with a means suitable on a chromate film. If this paint film is subsequently baked and desiccation and bridge formation of an epoxy resin are performed, the organic resin coat which is made into the purpose and which constructed the bridge will be obtained. stoving temperature -- general -- 80-290 \*\* -- desirable -- It is 120 - 200 \*\* extent. However, proper stoving temperature is determined by the crosslinking reaction temperature by the combination of the cross linking agent to add and base resin. A base material steel plate is a printing hardening mold. (BH) When it is a steel plate, it is desirable to make stoving temperature below into 150 \*\* so that printing hardenability may not be checked.

[0031] (5) Make MCA MCA (melamine cyanuric acid addition product) contain in an organic resin coat. MCA is a white impalpable powder crystal with a particle size [ first / an average of ] of about 1-2 micrometers, and is considered to have the chemical structure shown in attached drawing 1 . Although this compound has lubricating properties and it was known conventionally that it is useful as a solid lubricant, it was not known that it is effective also in the improvement of electropainting nature.

[0032] When MCA was made to contain in an organic resin coat, it became clear that electropainting of the organic compound surface treated steel sheet obtained could be carried out now by the almost same thickness as the case where cation electropainting nature has been remarkably improved compared with the conventional surface treated steel sheet of the same kind, with good corrosion resistance and spot welding nature held, and electropainting is carried out to a naked plating steel plate. The reason is considered as follows.

[0033] A hydrophilic property is very strong, and makes easy osmosis in the organic resin coat of an electrodeposition paint, and MCA can demonstrate the effectiveness of reducing the electric resistance of an organic resin coat at the time of electropainting. and since MCA distributes and exists by the shape of a particle in an organic resin coat, the effectiveness of making an electrodeposition paint permeating organic plastic paint like a hydrophilic polyamide into a resin coat compared with meltable hydrophilic resin at the time of electropainting is alike and large, and since more energization pass is securable, electropainting nature is improved remarkably.

[0034] Even if the part where organic resin coats and chromate films, such as that result, for example, the press crack care-and-cleaning section etc., are shaved off exists, it becomes possible to acquire the paint appearance an electrodeposited paint film is formed and it can fully be satisfied with thickness uniform to extent a difference with this part is not accepted to be of an appearance as an object for automobile sheathing external surface.

[0035] And it is the sliding nature at the time of press forming of an organic resin coat by the lubrication engine performance which MCA originally has. (press-forming nature) It is sharply improvable. By this invention, by making an organic resin coat contain a polyolefine wax in addition to MCA, if a base material remains as it is, in spite of being the bright steel sheet in which press forming is impossible, the organic compound surface treated steel sheet which can carry out press forming easily is obtained.

[0036] The loadings of MCA in an organic resin coat receive the weight of a desiccation coat. It considers as 0.1 - 20% of the weight of within the limits. The loadings of MCA are 0.1. If the improvement effect of desired electropainting nature and sliding nature is not acquired but it exceeds 20 % of the weight, when it will become difficult for a problem to arise at the distributed stability of MCA in the inside of the resin liquid used for spreading, and to distribute MCA in a coat at homogeneity, it is economically disadvantageous at under weight %. Addition of desirable MCA It is 0.5 - 15 % of the weight.

[0037] (6) Since a polyolefine wax base material steel plate is a bright steel sheet, the organic compound surface treated steel sheet obtained cannot secure sliding nature required for press forming only by blending MCA with an organic resin coat. Therefore, in order to improve further the sliding nature at the time of press forming, it adds to MCA and is a polyolefine wax. (an example, polyethylene wax) It blends with an organic resin coat.

[0038] The loadings of the polyolefine wax in an organic resin coat are 1 - 15% of the weight of within the limits preferably one to 20% of the weight to desiccation coat weight. At less than 1 % of the weight, if press forming of a surface treated steel sheet is difficult and exceeds 20 % of the weight also by concomitant use with MCA, the adhesion of an electrodeposited paint film will come to fall.

[0039] (7) As the silica above-mentioned was carried out, in order to improve the low-temperature-proof chipping nature of the surface treated steel sheet of this invention which uses a zinc system plating steel plate as a base material, make both a chromate film, and organic resin both [ one side or ] on it contain a silica. Although the mechanism by which the low-temperature-proof chipping nature of the organic compound surface treated steel sheet obtained by content of a silica is improved remarkably is not necessarily clear, it is thought that it is because distribution and absorption of a certain striking energy take place when a silica particle exists.

[0040] \*\* As a silica blended into the silica chromate film in a chromate film, it is a silica sol. (aquosity colloidal silica) Fumed silica (gaseous-phase colloidal silica) Any are sufficient. The silica to be used has that desirable whose first [ an average of ] particle size of a particle is 5-50mmicro.

[0041] the case where a silica is blended with a chromate film -- the silica content in a coat -- a  $\text{SiO}_2/\text{Cr}$  weight ratio -- 0.05-4.0 -- desirable -- 0.1-3.0 It considers as the becoming amount. Less than 0.05 are not enough as the improvement effect of low-temperature-proof chipping nature, and, on the other hand, this ratio is 4.0. If it exceeds, the insulation of a chromate film will serve as size and spot welding nature will fall. (the chip damage at the time of welding and energization impossible become easy to happen) .

[0042] \*\* Although both a silica sol and fumed silica can be applied when blending a silica into the silica organic resin coat in an organic resin coat, it is more desirable to use the silica sol excellent in especially weldability and corrosion resistance. A desirable silica sol is a thing within the limits whose first [ an average of ] particle size of a silica particle is 2-20mmicro. When blending a silica with an organic resin coat, the silica ( $\text{SiO}_2$ ) content in a desiccation coat makes it contain five to 40% of the weight, so that it may become 5 - 30% of the weight of an amount preferably. If a desired low-temperature-proof chipping nature improvement effect is not acquired but this amount, on the other hand, exceeds 40 % of the weight at less than 5 % of the weight, the fall of spot welding nature will be caused like the above.

[0043] (8) As stated to the silane coupling agent point, a silane coupling agent can be blended with both a chromate film, and organic resin both [ one side or ] as an arbitration addition component. Since the adhesion between each coat of plating / clo mate / organic resin and adhesion with an electrodeposited paint film will improve as a result of adhesion with the coat component of the silica particle in a coat increasing if a silane coupling agent is blended, much more good result is obtained by the improvement of low-temperature-proof chipping nature. Therefore, when a chromate film and/or an organic resin coat are made to contain a silica, a silane coupling agent may be blended collectively.

[0044] As for the loadings of a silane coupling agent, it is desirable to consider as 1x10 to 5 or more times to the weight of the silica made to contain in a chromate film or an organic resin coat. What is necessary is just to choose the class of silane coupling agent from the existing thing suitably.

[0045]

[Example] Next, this invention is illustrated according to an example. Among an example, % is weight %, as long as there is no assignment especially.

[0046] Example 1 both sides are  $R_a=0.14$ micrometer and  $R_a=0.8$ . Two kinds of cold rolled sheet steel of mum (board thickness 0.8mm) It receives and is Zn-13%nickel alloy electroplating to both sides. (sulfate bath) It gave. the amount of superintendent officers of this plating coat -- per one side -- 30 g/m<sup>2</sup> it was .

[0047] On a double-sided plating coat, it is a gaseous-phase silica at the weight ratio of  $\text{SiO}_2/\text{Cr}=1$ . (first



[ an average of ] particle size 15  $\mu$ m) The spreading mold coating liquid to contain is applied by bar coater so that the chromate film of 60 mg/m<sup>2</sup> may be formed by metal Cr conversion, and whenever [ board temperature ] 150 degrees C was heated for 60 seconds like, and the chromate film was formed. [0048] On this chromate film, by bar coater, thickness is changed, and is applied and whenever [ board temperature ] the coating liquid which uses an urethane modified epoxy resin as a principal component, and contains block isocyanate as a cross linking agent Heat for 60 seconds, dried the paint film, resin was made to construct a bridge so that it may become 150 degrees C, and the organic compound surface treated steel sheet was obtained. In addition to the above-mentioned resin and a cross linking agent, either 4% of MCA or 20% of hydrophilic polyamide resin and 10% of polyethylene wax are blended to nonvolatile matter sum total weight, before use, it fully stirred in the used coating liquid, and it was distributed.

[0049] The cation electropainting nature of each obtained organic compound surface treated steel sheet was examined as follows. Each trial steel plate to 150 mmx70 mm A test piece is cut down and it is only the one half (75 mmx70 mm) of the one side 600 It ground with the abrasive paper of watch, the resin coat and the chromate film were removed, and the plating side was exposed. Subsequently, after performing phosphoric-acid zinc processing to this whole field as a paint substrate, the commercial cation electrodeposition paint was used, cation electropainting was performed on the conditions by which the electrodeposited paint film of 18 micrometers of thickness is formed in the polish section, and the thickness of the electrodeposited paint film of the non-grinding section when the electrodeposited paint film of 18-micrometer thickness is formed in the polish section was measured. It is estimated that electropainting nature is good, so that the difference of the thickness of an electrodeposited paint film is small in the polish section and the non-grinding section.

[0050] A test result is shown in drawing 2 as relation between organic resin coat thickness and the electrodeposited film thickness of the non-grinding section. As shown in this drawing, when electropainting of the surface treated steel sheet which made the hydrophilic polyamide resin proposed by JP,3-32638,B contain in an organic resin coat was carried out, the electrodeposited film thickness difference of the polish section and the non-grinding section was large, and this electrodeposited film thickness difference became so large that the thickness of an organic resin coat is large. Therefore, in the care-and-cleaning sections, such as a press crack equivalent to the polish section, an electrodeposited paint film becomes thin and appearance nonuniformity will occur after electropainting.

[0051] On the other hand, when MCA was made to contain in an organic resin coat by this invention, electropainting could be carried out to the thickness of an organic resin coat by the thickness as the polish section also with the non-grinding section same related always, and it excelled in electropainting nature. Even if this has the care-and-cleaning section of a press crack etc., it means that producing appearance nonuniformity after electropainting is lost.

[0052] In addition, for the difference in Ra of a base material steel plate, Ra of the base material steel plate which did not influence electropainting nature but was used is 0.14 micrometers and 0.8. Even if it was any of  $\mu$ m, the almost same result was obtained. The case where Ra was 0.14 micrometers showed drawing 2.

[0053] Furthermore, the thickness of the organic resin coat containing MCA About the trial steel plate which is 0.5 micrometers, the coating for automobiles of marketing after the above-mentioned electropainting is used, and it is middle-coat paint. (35 micrometers of thickness) And finishing paint (35 micrometers of thickness) It gives and is a portable visibility glossmeter about the paint image clarity of the non-grinding section. (PGD IV mold) It measured. consequently, PGD at the time of using a Ra=0.14micrometer steel plate as a base material a value -- 0.9 it was -- a thing -- receiving -- Ra=0.8 PGD at the time of using the steel plate of  $\mu$ m as a base material a value -- 0.7 it was . When the small steel plate of Ra was clearly used as the base material, the image clarity after paint improved remarkably.

[0054] The organic compound surface treated steel sheet was produced like the example 1 by using example 2Ra=0.14micrometer cold rolled sheet steel as a base material. However, an organic resin coat is made to contain MCA at a various rate, and the thickness is 1.0. It fixed with  $\mu$ m. About the result

of having examined the electropainting nature of the obtained organic compound surface treated steel sheet like the example 1, it is an MCA content in an organic resin coat. (MCA addition to the nonvolatile matter total quantity of coating liquid) It is shown in drawing 3 as relation of the electrodeposited film thickness in the receiving non-grinding section.

[0055] It became clear that it became possible if MCA is made to contain in the amount more than 0.1 % in an organic resin coat to carry out electropainting by the same thickness as the polish section from the result shown in drawing 3, and the outstanding electropainting nature could be demonstrated now.

[0056] Example 3 both sides are Ra=0.14micrometer cold rolled sheet steel. (board thickness 0.7 mm) It considered as the base material and the organic compound surface treated steel sheet was produced like the example 1. The used base material steel plate had TS=300 N/mm<sup>2</sup>, YP=130 N/mm<sup>2</sup>, and El=47% tractive characteristics. The amount of superintendent officers of a Zn-13%nickel alloy-plating coat is 20 g/m<sup>2</sup> per one side. It carried out, and the chromate film which contains a silica by the weight ratio of SiO<sub>2</sub>/Cr=1 on it was formed so that it might become the coating weight of 50 mg/m<sup>2</sup> by metal Cr conversion. The organic resin coat layer of the maximum upper layer is the content (addition to the nonvolatile matter total quantity in coating liquid) of MCA and polyethylene wax. It was made to change and formed.

[0057] About the press-forming nature of the obtained organic compound surface treated steel sheet, it is a contraction ratio 2.0. The existence of crack generating by cupping trial estimated. Moreover, in order to evaluate the secondary adhesion of an electrodeposited paint film, it is the test piece of each surface treated steel sheet. (un-grinding) Cation electropainting was performed after phosphoric-acid zinc processing on the conditions in which the electrodeposited paint film of 20 micrometers of thickness is formed to the Zn-13%nickel alloy-plating steel plate of a base material. It is this electropainting test piece in 50-degree C warm water 240 \*\*\*\* trial after carrying out time amount immersion (1mm spacing x100 a mass, cellophane tape exfoliation) It gave and the paint film survival rate estimated secondary adhesion.

[0058] A test result is shown in the next table 1 with MCA in an organic resin coat, and the content of a wax. When the organic resin coat contained both more than MCA0.1 % and beyond polyethylene wax 1% according to this invention, good press forming without a crack was possible so that this test result might show, but when at least one side of these addition component was missing, the crack occurred at the time of press forming. That is, in using a bright steel sheet as a base material, it turns out that an organic resin coat needs to contain both MCA and wax. However, although press-forming nature was secured when the content of a wax exceeded the upper limit which is 20%, the adhesion of an electrodeposited paint film fell.

[0059]

[Table 1]

試験 No.	MCA 含有量	ワックス 含有量	プレス 成形性	電着塗膜 二次密着性	区 分
1	0 %	0 %	割れ	100%	比較例
2	0.1%	0 %	割れ	100%	比較例
3	0 %	1 %	割れ	100%	比較例
4	0.1%	1 %	良好	100%	本発明
5	0.1%	20%	良好	100%	本発明
6	0.1%	30%	良好	90%	比較例

[0060] Example 4 both sides are Ra=0.18micrometer cold rolled sheet steel (board thickness 0.8 mm). It received and the Zn-13%nickel alloy plating of the amount of superintendent officers or Zn-9%Fe alloy



plating shown in Table 2 was performed to both sides with electroplating by the sulfate bath. Then, by the same approach as an example 1, the organic resin coat which uses a spreading mold chromate film and epoxy system resin as a principal component was formed on the plating coat, and the organic compound surface treated steel sheet was produced. Coating weight of a chromate film (Cr conversion) The thickness of a resin coat was changed as shown in Table 2.

[0061] In the used chromate liquid, it is colloidal silica by the case. (first [ an average of ] particle size 10 m micro) Silane coupling agent (gamma-chlorosilane SHIDOKISHI propyltrimethoxysilane) One side or both were added. Addition of a silica ( $\text{SiO}_2/\text{Cr}$  weight ratio) Addition of a silane coupling agent (pair  $\text{SiO}$  duplex quantitative ratio) It is shown in Table 2.

[0062] The coating containing the block isocyanate of the bisphenol A system epoxy resin and a cross linking agent is made to distribute 5% of MCA, and 3% of polyethylene wax to the nonvolatile matter total quantity, and the coating liquid used for formation of an organic resin coat is a silica sol by the case further. (first [ an average of ] particle size 10 m micro) Both both [ same / the same one side or ] as a top were blended.  $\text{SiO}_2$  addition to this coating liquid (% to a nonvolatile matter) Addition of a silane coupling agent (pair  $\text{SiO}$  duplex quantitative ratio) It is as being shown in Table 2.

[0063] The low-temperature-proof chipping nature, Cr elution volume, external surface-proof \*\*\*\*, and spot welding nature of the obtained organic compound surface treated steel sheet were investigated with the following test method. A test result is also shown according to Table 2.

[0064] (Low-temperature-proof chipping nature) After painting two quart 2 BEKU of 30 micrometers of electropainting, and 40 micrometers of automobile top coat to a test piece, it cooled at -20 degrees C, an impact of a pebble was given with the GURABERO circuit tester, and this part was exfoliated on the cellophane tape. The diameter of exfoliation in the plating / steel plate interface after exfoliation was measured.

[0065] (Cr elution volume) It is 40-degree C alkaline-degreasing liquid about a test piece. (FC4410 by Nihon Parkerizing Co., Ltd.) It degreased by having been immersed for 2 minutes in inside, Cr coating weight of the test piece before and behind that was measured with fluorescence X rays, and Cr elution volume was computed.

[0066] (External surface-proof \*\*\*\*) The cross-cut crack of the depth which reaches a base material steel plate with a cutter knife after painting two quart 2 BEKU of 30 micrometers of electropainting and 40 micrometers of automobile top coat to a test piece was put in, and after carrying out an outdoor exposure including two salt water spraying per week for three months, the existence of rust generating from the cut section was judged visually.

[0067] (Spot welding nature) Alternating current single-spot-welding machine which piled up two test pieces of the same organic compound surface treated steel sheet, and was equipped with the electrode tip made from a Cu-Cr alloy of 6mm of diameters of a tip (50 Hz) It used and the spot welding continuation RBI trial was performed on condition that welding current 10 kA, 20 cycle squeeze time, the 12 cycle resistance welding time, 5 cycle maintenance, and welding-pressure 200 Kg. It had the number of RBIs which welding peeling produced in shear tension, and spot welding nature was evaluated.

[0068]

[Table 2]

区分	試験No	亜鉛系めっき		クロメート皮膜			エポキシ系樹脂皮膜			耐低温 チップング性 (ぬき剥離径) (mm)	Cr溶出量 (mg/m <sup>2</sup> )	耐外面錆性	スポット 溶接性 (打点数)
		めっき種	付着量 (g/m <sup>2</sup> )	Cr付着量 (mg/m <sup>2</sup> )	SiO <sub>2</sub> /Cr 重量比	シランカップ 剤量 <sup>1)</sup>	膜厚 (μm)	SiO <sub>2</sub> 量 (wt%)	シランカップ 剤量 <sup>1)</sup>				
本発明例	1	Zn-13%Ni	10	40	0.4	1×10 <sup>-4</sup>	0.5	5	0	0.2	0.2	赤錆発生なし	>5000
	2		20	20	0.6	1×10 <sup>-3</sup>	0.5	8	1×10 <sup>-4</sup>	0.3	0.6	赤錆発生なし	>5000
	3		20	190	0.07	0	0.5	12	0	0.3	2.0	赤錆発生なし	>5000
	4		30	60	3.8	1×10 <sup>-5</sup>	0.4	18	1×10 <sup>-5</sup>	0	1.0	赤錆発生なし	4100
	5		30	50	0.9	0	1.9	20	0	0	0.5	赤錆発生なし	3500
	6		20	30	1.2	0	0.8	35	0	0.2	0.3	赤錆発生なし	3500
	7		30	70	0	0	1.8	25	0	0.2	0.1	赤錆発生なし	3500
	8	Zn-9%Fe	35	30	0.6	0	0.6	10	0	0	0.8	赤錆発生なし	>5000
	9		45	60	0.6	0	0.5	0	0	0.3	0.6	赤錆発生なし	>5000
比較例	10	Zn-13%Ni	30	0*	0	0	0*	0	0	3.6	0	赤錆発生なし	>5000
	11		0*	50	0.5	1×10 <sup>-5</sup>	0.7	10	1×10 <sup>-5</sup>	0.1	0.1	赤錆発生あり	>5000
	12		30	10*	0.5	1×10 <sup>-3</sup>	0.7	10	1×10 <sup>-4</sup>	2.1	0.2	赤錆発生なし	>5000
	13		30	250*	0.5	1×10 <sup>-3</sup>	0.7	10	1×10 <sup>-4</sup>	0	4.8	赤錆発生なし	4200
	14		30	70	5.0*	1×10 <sup>-5</sup>	0.4	15	1×10 <sup>-5</sup>	0.1	0.1	赤錆発生なし	2000
	15		30	50	0.5	0	0.01*	15	0	0.9	4.7	赤錆発生なし	>5000
	16		30	50	0.5	0	3.0*	15	0	0.1	0.1	赤錆発生なし	0(不能)
	17		20	50	0*	0	1.0	0*	0	3.2	0.1	赤錆発生なし	>5000
	18		20	50	0.5	0	1.0	50*	0	0.1	0.1	赤錆発生なし	2500

(注) \* 本発明の範囲外； 1) シランカップリング剤量は (シランカップリング剤D)/(SiO<sub>2</sub>) の重量比。

[0069] As shown in Table 2, the organic compound surface treated steel sheet by this invention was excellent in any examined engine performance. on the other hand -- the example of a comparison -- the coating weight of a chromate film, or the thickness of an organic resin coat -- this invention -- being out

of range -- or -- a chromate film and an organic resin coat -- both did not contain a silica or the content of the silica showed the example with this invention out of range. In these examples of a comparison, at least one engine performance of low-temperature-proof chipping nature, Cr elution volume, external surface-proof \*\*\*\*, and spot welding nature was inferior, and the organic compound surface treated steel sheet which fills all engine performance was not able to be obtained. In addition, each electropainting nature of the organic compound surface treated steel sheet produced by this example was good.

[0070]

[Effect of the Invention] It is  $Ra \leq 0.3$  which was not used until now since press forming was difficult although the organic compound surface treated steel sheet of this invention was ideal for the improvement of image clarity as explained in full detail above. A bright steel sheet is succeeded in raising the sliding nature of a coat to extent in which press forming good also as a base material is possible by using the bright steel sheet of mum as a base material, and making the organic resin coat of the maximum upper layer contain both MCA and polyolefine wax. It enabled this to attain the image clarity after the outstanding paint conventionally beyond level originating in a bright steel sheet.

[0071] and cation electropainting nature and low-temperature-proof chipping nature be also improve remarkably, and the organic compound surface treated steel sheet for automobiles which can fill all the engine performance require of inside and outside both sides of the steel plate for automobile sheathing be obtain, hold the outstanding corrosion resistance and spot welding nature according to an operation of the silica which either [ at least ] MCA which exist in the organic resin coat which consist of bridge formation epoxy system resin, this resin coat or a lower layer chromate film be make to contain. Therefore, if an automobile car body is manufactured from the surface treated steel sheet of this invention, the remarkable improvement in the appearance of an automobile and endurance can be expected, and very useful effectiveness will be brought about on industry.

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[Translation done.]

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1. This document has been translated by computer. So the translation may not reflect the original precisely.
2. \*\*\*\* shows the word which can not be translated.
3. In the drawings, any words are not translated.

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**DESCRIPTION OF DRAWINGS**

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[Brief Description of the Drawings]

[Drawing 1] MCA (melamine cyanuric acid adduct) The chemical structure is shown.

[Drawing 2] It is the graph which shows the electropainting nature of an organic compound surface treated steel sheet which has an organic resin coat containing a hydrophilic polyamide or MCA as relation between organic resin coat thickness and the electrodeposited film thickness of the non-grinding section.

[Drawing 3] It is the graph which shows the electropainting nature of an organic compound surface treated steel sheet which has an organic resin coat containing MCA as relation between the MCA content in an organic resin coat, and the electrodeposited film thickness of the non-grinding section.

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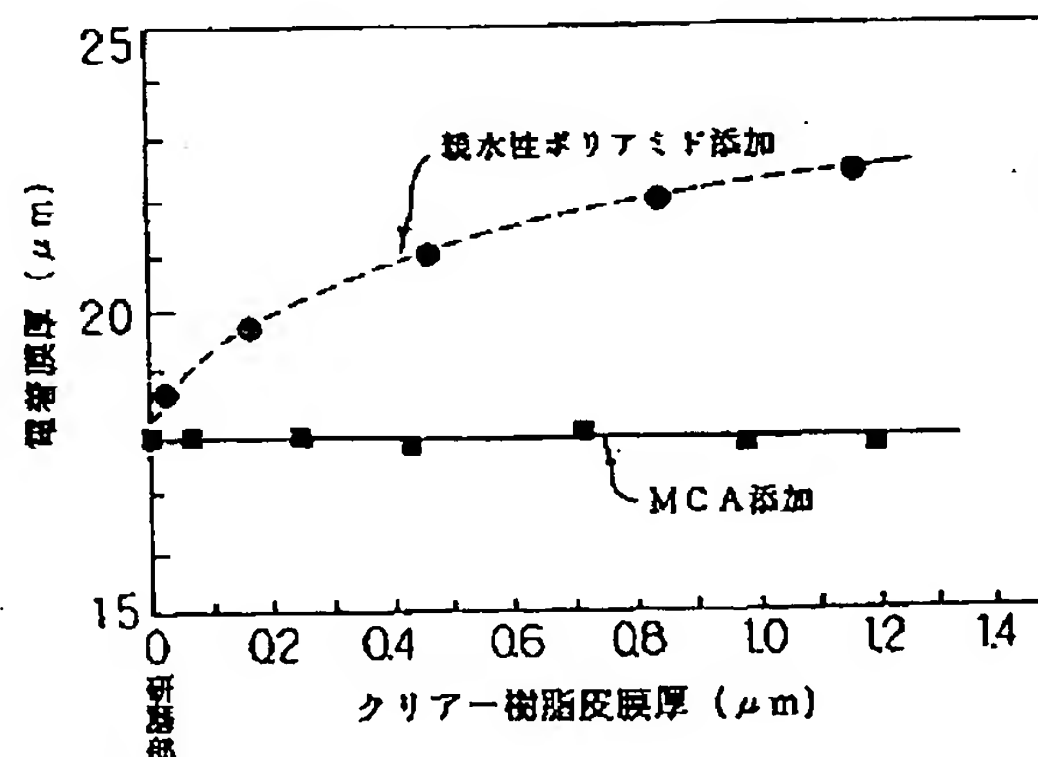
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(54)【発明の名称】 自動車用表面処理鋼板

(57)【要約】

【目的】 亜鉛または亜鉛合金めっき(例、Zn-Ni、Zn-Fe)鋼板上にクロメート皮膜と有機樹脂皮膜とを設けた有機複合表面処理鋼板において、自動車外装鋼板の内外面に要求される各種の性能(耐食性、プレス成形性、スポット溶接性、カチオン電着塗装性、耐低温チップング性、塗装後鮮映性)を全て満たす。

【構成】 少なくとも片面側の表面粗度がRaで0.3  $\mu$ m以下のブライト鋼板を基材として使用。最上層は、0.1~20重量%のメラミンシアヌル酸付加物と1~20重量%のポリオレフィンワックスを含有する、膜厚0.1~2.0  $\mu$ mの架橋エポキシ系樹脂皮膜とする。シリカを、クロメート皮膜中にSiO<sub>2</sub>/Cr重量比で0.05~4.0となる量で含有させるか、および/または有機樹脂皮膜中に5~40重量%のSiO<sub>2</sub>量で含有させる。



## 【特許請求の範囲】

【請求項1】 少なくとも鋼板の片面側が、Raで0.3  $\mu\text{m}$ 以下の表面粗度を有し、この表面上に下層から順に

①亜鉛または亜鉛合金めっき層、

②金属Cr換算で20~200  $\text{mg}/\text{m}^2$  のクロメート皮膜、

③0.1~20重量%のメラミンシアヌル酸付加物および1~20重量%のポリオレフィンワックスを含有する架橋エポキシ系樹脂からなる、膜厚0.1~2.0  $\mu\text{m}$ の有機樹脂皮膜、を有し、さらにクロメート皮膜がシリカを $\text{SiO}_2/\text{Cr}$ 重量比で0.05~4.0となる量で含有するか、および/

または有機樹脂皮膜がシリカを5~40重量%の $\text{SiO}_2$ 量で含有することを特徴とする、自動車用表面処理鋼板。

## 【発明の詳細な説明】

## 【0001】

【産業上の利用分野】本発明は、優れたカチオン電着塗装性を示し、塗装後の鮮映性が著しく改善され、しかも耐食性、耐低温チップング性、スポット溶接性、プレス成形性などの自動車用鋼板に要求される他の特性も良好な自動車用表面処理鋼板に関する。

## 【0002】

【従来の技術】近年、自動車車体の防錆性能への要求は年を追って厳しさを増しており、この要求に対処すべく、多様な表面処理鋼板が開発されてきた。最近、特に自動車の外装外面に対する防錆性能強化策の一環として、亜鉛めっき又は亜鉛合金めっき(例、Zn-NiもしくはZn-Fe合金めっき等)鋼板を母材とし、これにクロメート処理とクリヤー塗料(例、架橋剤を含有するエポキシ系樹脂塗料)による薄い有機樹脂被覆を施した、有機複合表面処理鋼板の適用が急速に進められている。

【0003】ところが、従来の有機複合表面処理鋼板は、上層の有機樹脂皮膜の導電性が悪いため、薄膜にしてもカチオン電着塗装性が十分ではなかった。防錆性能と並んで自動車外観に対する要求も今後ますます高度化することが予想されるため、外観に影響する電着塗装性の改善が急務となっていた。

【0004】有機複合表面処理鋼板の電着塗装性の改善策として、特公平3-32638号公報には、上層の有機樹脂皮膜を、親水性ポリアミド樹脂を含むエポキシ系樹脂から形成することが提案されている。この表面処理鋼板は、従来品に比べると確かに優れたカチオン電着塗装性を示し、自動車内板用として考えた場合には満足できる性能を備えたものであったが、外板用として使用すると次のような問題点があり、自動車外装用としては不適であると言わねばならなかった。

【0005】即ち、この有機複合表面処理鋼板にカチオン電着塗装を施すと、この表面処理鋼板の母材として用いた亜鉛系めっき鋼板を裸のまま同一条件下でカチオン電着塗装した場合に比べて、電着塗装膜厚が1~8  $\mu\text{m}$ 程度厚くなってしまう。このため、自動車用外板として用いた場合、プレス疵手入れ部のように有機樹脂皮膜や

クロメート皮膜が削り取られている部位では、その周囲より電着塗装膜厚が薄くなり、塗装外観が著しく低下する。

【0006】これとは別に、従来の有機複合表面処理鋼板は耐低温チップング性が十分でないという問題点も指摘されていた。有機複合表面処理鋼板の耐食性は主に最下層の亜鉛または亜鉛合金めっき皮膜により確保されるが、亜鉛系のめっき皮膜はめっき時に生じた大きな残留応力を保持したままであるので、低温チップング(欧州や北米などの寒冷地で石はね等の衝撃によりめっき層が鋼板との界面から剥離する現象)を生じ易いという傾向があった。自動車外装用の表面処理鋼板にとって、自動車の耐食性を著しく劣化させ、寿命や外観の悪化につながる低温チップングの防止は重要である。

【0007】この問題の対策として、特開昭46-78832号公報には、亜鉛系めっき表面に緩衝材として有効な軟質(ガラス転移点55℃以下)の樹脂皮膜を形成することが提案されている。しかし、軟質樹脂は架橋エポキシ系樹脂などに比べて耐食性が低いので、表面処理鋼板の主目的である耐食性改善が不十分となる。さらに、上記と同様、電着塗装の厚膜化による外観不良という問題も免れえなかった。

【0008】自動車の外観を左右する重要な要素は、塗装後の鮮映性である。従来から、塗装後の鮮映性を向上させる手段として、レーザー加工を施したロールで鋼板を圧延して、ダルパターンを形成する技術が知られている(例、特開昭62-168602号公報など)。この技術は、鋼板の平坦をある程度確保しつつ、プレス成形時の潤滑に必要な油保持性を付与するためにダル化するものである。塗装後の鮮映性にとって、ダルのない、いわゆるブライト鋼板が理想的であると考えられるにもかかわらず、ブライト鋼板では油保持性がなく、プレス成形が不可能であることから、鋼板表面に凹凸のあるダルを形成せざるを得なかった。

## 【0009】

【発明が解決しようとする課題】本発明の目的は、自動車外装材の内面側および外面側に要求される全ての性能を満たした、自動車用の有機複合表面処理鋼板を提供することである。

【0010】本発明の具体的な目的は、優れた耐食性、プレス成形性、スポット溶接性を備えているのは勿論、カチオン電着塗装性、耐低温チップング性、塗装後の鮮映性についても著しく改善された、自動車用の有機複合表面処理鋼板を提供することである。

## 【0011】

【課題を解決するための手段】本発明者らは、鮮映性の改善に理想的な基材である $\text{Ra} \leq 0.3 \mu\text{m}$ の鋼板(いわゆるブライト鋼板)を基材として、その表面に潤滑性に優れた有機樹脂皮膜を形成することにより、プレス成形可能で、上記の各種の性能を満たす有機複合表面処理鋼

板を得るべく検討を重ねた結果、本発明に到達した。

【0012】ここに、本発明は、少なくとも鋼板の片面側が、 $Ra$ で $0.3\ \mu m$ 以下の表面粗度を有し、この表面上に下層から順に

①亜鉛または亜鉛合金めっき層、

②金属Cr換算で $20\sim 200\ mg/m^2$ のクロメート皮膜、

③ $0.1\sim 20$ 重量%のメラミンシアヌル酸付加物および $1\sim 20$ 重量%のポリオレフィンワックスを含有する架橋エポキシ系樹脂からなる、膜厚 $0.1\sim 2.0\ \mu m$ の有機樹脂皮膜、を有し、さらにクロメート皮膜がシリカを $SiO_2/Cr$ 重量比で $0.05\sim 4.0$ となる量で含有するか、および/または有機樹脂皮膜がシリカを $5\sim 40$ 重量%の $SiO_2$ 量で含有することを特徴とする、自動車用表面処理鋼板を要旨とする。

【0013】本発明の有機複合表面処理鋼板の主要な特徴は次の(a)～(e)にある。

(a) 塗装後鮮映性の究極的な改善を目指して、基材鋼板にブライツ鋼板を採用する。

(b) 下地の亜鉛系めっき層と中間のクロメート皮膜に加えて、最表層の樹脂皮膜を緻密で硬質の架橋エポキシ樹脂皮膜とし、耐食性を改善する。

(c) この樹脂皮膜中に潤滑性に優れたメラミンシアヌル酸付加物(以下、MCAと略記)とポリオレフィンワックスを添加して皮膜に高度の摺動性を付与する。その結果、ブライツ鋼板が基材であっても容易にプレス成形が可能となる。

(d) 樹脂皮膜中に配合したMCAの効果により、耐食性やスポット溶接性を低下させずに、電着塗装性も著しく改善される。

(e) 亜鉛系めっき層の低温チッピングの問題については、クロメート皮膜と樹脂皮膜の一方または両方にシリカを配合して耐低温チッピング性を改善する。

【0014】以上の総合的な結果として、カチオン電着塗装性と塗装後鮮映性が著しく改善され、耐食性、耐低温チッピング性、スポット溶接性、プレス成形性などの自動車用鋼板の内面および外面に要求される各種の性能をすべてについて満足できる有機複合表面処理鋼板が得られるのである。

【0015】

【作用】本発明の有機複合表面処理鋼板において上記構成を採用した理由をその作用と共に次に説明する。

【0016】(1) 基材鋼板

塗装後の鮮映性確保に理想的材料である表面粗度が $Ra\leq 0.3\ \mu m$ の鋼板(ブライツ鋼板)を適用する。従来は、油保持性がなく、プレス成形ができないことから、ブライツ鋼板は基材鋼板として不適当であるとされていたが、本発明では上層の有機樹脂皮膜に高度の潤滑性を付与することにより、ブライツ鋼板の適用が可能となった。鋼板の表面粗度が $Ra$ で $0.3\ \mu m$ を超えると、塗装後鮮映性の改善効果が不明確となる。

【0017】鮮映性は外面側に要求される性能であるから、片面のみが上記表面粗度を有していればよいが、製造工程の都合で両面とも $Ra\leq 0.3\ \mu m$ のブライツ鋼板であってもよい。以下に説明する、めっき+クロメート皮膜+有機樹脂皮膜からなる多層の表面処理被覆は、基本的には外面側片面に形成されていれば良く、プレス性もダイス面側の摺動性を改善することで大幅に向上することから、外面側片面だけで効果は十分発揮されるが、内面側に要求される耐孔あき性等も改善されることから、両面に適用することもできる。

【0018】(2) 下地めっき

有機複合表面処理の最下層となる下地めっきは、耐食性確保のため、犠牲防食能に優れた亜鉛または亜鉛合金めっき(以下、亜鉛系めっきという)の皮膜とする。即ち、本発明の表面処理鋼板の母材鋼板としては、亜鉛系めっきが施された亜鉛系めっき鋼板を使用する。この亜鉛系めっきの目付け量は、耐食性の要求レベルに応じて選択されるが、耐外面錆性を向上させる目的からは、片面当たり $10g/m^2$ 以上とすることが好ましい。目付け量が多すぎるとプレス成形性が低下するので、上限は $60g/m^2$ 程度とするのが好ましい。

【0019】亜鉛合金めっきの種類は特に限定されず、 $Zn-Ni$ 合金めっき、 $Zn-Fe$ 合金めっき、 $Zn-Al$ めっき、或いはさらに $Co$ 、 $Ti$ などを添加した公知の亜鉛系合金めっきのいずれを適用しても構わない。亜鉛系めっきの方法も特に制限されない。目付け量が比較的少なくてよいことから、電気めっきが好ましいが、溶融めっきや合金化溶融亜鉛めっきでもよい。また、亜鉛系めっき皮膜は、2層以上の複層めっき皮膜であってもよい。

【0020】(3) クロメート皮膜

亜鉛系めっき層の上にクロメート皮膜を設ける。クロメート皮膜には、亜鉛系めっき鋼板を基材とする表面処理鋼板の耐食性をさらに改善する作用がある。また、クロメート皮膜にシリカを含有させると、耐低温チッピング性を向上させる作用も発揮する。クロメート皮膜の形成方法は、塗布型、反応型、電解型のいずれも可能であるが、耐食性に特に優れた塗布型クロメート皮膜が好ましい。

【0021】クロメート皮膜中には、任意に添加できるシリカの他に、従来よりクロメート皮膜に添加されてきた他の添加剤を配合することもできる。かかる添加剤の例としては、シランカップリング剤、防錆顔料、リン酸、フッ化水素酸などがある。

【0022】クロメート皮膜の付着量は、金属Cr換算で、 $20\sim 200\ mg/m^2$ とする。 $20\ mg/m^2$ 未満では、自動車外装用に必要なレベルの耐食性や耐低温チッピング性を確保することができず、付着量が $200\ mg/m^2$ を超えると、プレス成形性や溶接性が劣化する上、塗装前の脱脂・化成処理時のCr溶出量が多くなる。クロメート皮膜の好ましい付着量は、 $20\sim 150\ mg/m^2$ である。



## 【0023】(4) 有機樹脂皮膜

クロメート皮膜の上の有機樹脂皮膜(クリアー皮膜)は、表面処理鋼板の脱脂・化成処理時において下層のクロメート皮膜からCrが溶出するのを防止し、かつ外部から腐食性物質が侵入するのを妨げるバリアー層として機能すると同時に、電着塗膜との密着性を確保する作用と、プレス成形時に摺動性を付与する潤滑皮膜としての作用も果たす。本発明においては、緻密で耐食性に優れたエポキシ系樹脂を主成分とする架橋樹脂皮膜を利用する。

【0024】エポキシ系樹脂としては、ビスフェノールA系、ビスフェノールF系、ノボラック型、臭素化エポキシ等の任意のグリシジルエーテル型エポキシ樹脂、並びにこれらのエポキシ樹脂中のエポキシ基およびヒドロキシル基を乾性油脂脂肪酸中のカルボキシル基と反応させたエポキシエステル樹脂、イソシアネートと反応させることにより得られるウレタン変性エポキシ樹脂などの各種変性エポキシ樹脂も使用できる。さらには、2価フェノール(例、レゾルシンおよび/またはビスフェノール類)をアルカリ触媒の存在下にほぼ等モル量のエピハロヒドリンと重縮合させて得られるポリヒドロキシポリエーテル樹脂と総称される樹脂も、本発明のエポキシ系樹脂に含まれる。

【0025】このエポキシ系樹脂には、少量であれば、他の樹脂(例、アクリル樹脂、ポリエステル樹脂、アルキッド樹脂、ポリビニルブチラール樹脂、各種水溶性樹脂)を配合してもよい。

【0026】樹脂皮膜を緻密化して耐食性を改善するために、架橋剤によりエポキシ系樹脂を塗膜の加熱乾燥中に架橋させ、架橋樹脂皮膜とする。架橋剤としては、エポキシ樹脂用硬化剤として公知の、フェノール樹脂、アミノ樹脂、ポリアミド、アミノポリアミド、アミン、ブロックイソシアネート、酸無水物などが使用できる。架橋剤の添加量は、架橋したエポキシ系樹脂皮膜の可撓性が過度に失われないように選択する。

【0027】本発明においては、この架橋エポキシ系樹脂皮膜中にMCAとポリオレフィンワックスを含有させる。耐低温チッピング性の改善を図るために、さらにシリカを含有させてもよい。その他の任意添加成分もエポキシ系樹脂皮膜中に含有させることができる。例えば、シランカップリング剤、シリカ以外の無機充填材(例、各種ケイ酸塩鉱物、アルミナ、炭酸カルシウムなど)、金属クロム酸塩系防錆顔料(例、クロム酸バリウムもしくはストロンチウム)の1種もしくは2種以上を、有機樹脂皮膜の性能に悪影響を与えない範囲で添加することができる。

【0028】また、表裏の識別性を付与するなどの目的で、有機樹脂皮膜に有機もしくは無機着色顔料または染料を含有させて皮膜を着色してもよい。例えば、鋼板の片面のみに本発明の有機複合表面処理を施す場合(例、

自動車外装用の外面側のみを表面処理する場合)には、有機樹脂皮膜を着色することによって、表裏の識別が目瞭然となって、ユーザーでの作業が容易となる。

【0029】有機樹脂皮膜の膜厚は0.1~2.0  $\mu\text{m}$ とする。膜厚が0.1  $\mu\text{m}$ 未満では、上述した有機樹脂皮膜の作用効果が十分に得られない。膜厚が2.0  $\mu\text{m}$ を超えると、この皮膜の絶縁性が大きくなって、スポット溶接性が低下し、溶接時のチップの損傷や通電不能を引き起こす恐れがある。

- 10 【0030】有機樹脂皮膜の形成は、エポキシ系樹脂を必要であれば適当な有機溶剤で希釈して樹脂液を調製し、この樹脂液に架橋剤、MCA、ポリオレフィンワックスと、必要であれば他の添加成分(例、シリカゾル、シランカップリング剤など)を不揮発分(溶剤以外の全成分)の合計重量に対して所定の配合量となるように添加して溶解ないし分散させ、クロメート皮膜の上に適当な手段で塗布することにより行う。この塗膜を次いで焼付けて乾燥およびエポキシ樹脂の架橋を行うと、目的とする架橋した有機樹脂皮膜が得られる。焼付温度は一般に80~290  $^{\circ}\text{C}$ 、好ましくは120~200  $^{\circ}\text{C}$ 程度である。但し、適正な焼付温度は、添加する架橋剤とベース樹脂の組み合わせによる架橋反応温度により決定される。基材鋼板が焼付硬化型(BH)鋼板である場合には、焼付硬化性を阻害しないように、焼付温度を150  $^{\circ}\text{C}$ 以下とすることが好ましい。

【0031】(5) MCA(メラミンシアヌル酸付加物) MCAは有機樹脂皮膜中に含有させる。MCAは平均一次粒径1~2  $\mu\text{m}$ 程度の白色微粉末結晶であり、添付の図1に示す化学構造を有すると考えられている。この化合物が潤滑特性を有し、固体潤滑剤として有用であることは従来より知られていたが、電着塗装性の改善にも有効であることは知られていなかった。

【0032】MCAを有機樹脂皮膜中に含有させると、得られる有機複合表面処理鋼板は、良好な耐食性とスポット溶接性を保持したまま、従来の同種の表面処理鋼板に比べてカチオン電着塗装性が著しく改善され、裸のめっき鋼板に電着塗装した場合とほぼ同じ厚みで電着塗装することができるようになることが判明した。その理由は次のように考えられる。

- 40 【0033】MCAは親水性が非常に強く、電着塗料の有機樹脂皮膜への浸透を容易にし、電着塗装時に有機樹脂皮膜の電気抵抗を低下させる効果を発揮できる。しかも、MCAは有機樹脂皮膜中に微粒子状で分散して存在するため、親水性ポリアミドのような有機樹脂塗料に可溶な親水性樹脂に比べて、電着塗装時に電着塗料を樹脂皮膜中に浸透させる効果は格段に大きく、より多くの通電パスを確保できることから、電着塗装性が著しく改善される。

- 50 【0034】その結果、例えば、プレス疵手入れ部などのような有機樹脂皮膜やクロメート皮膜が削り取られて



いる部位が存在していても、この部位との差が認められない程度に均一な厚さで電着塗膜が形成され、自動車外装外面用として十分に満足できる塗装外観を得ることが可能となる。

【0035】しかも、MCAが本来有する潤滑性能により、有機樹脂皮膜のプレス成形時の摺動性（プレス成形性）も大幅に改善することができる。本発明では、MCAに加えてポリオレフィンワックスを有機樹脂皮膜に含有させることで、基材がそのままではプレス成形不可能なブライต์鋼板であるにもかかわらず、容易にプレス成形

することが可能な有機複合表面処理鋼板が得られるのである。

【0036】有機樹脂皮膜中におけるMCAの配合量は、乾燥皮膜の重量に対して0.1～20重量%の範囲内とする。MCAの配合量が0.1重量%未満では所望の電着塗装性および摺動性の改善効果が得られず、20重量%を超えると、塗布に用いる樹脂液中でのMCAの分散安定性に問題が生じ、MCAを皮膜中に均一に分布させることが困難となる上、経済的にも不利である。好ましいMCAの添加量は0.5～15重量%である。

【0037】(6) ポリオレフィンワックス  
基材鋼板がブライต์鋼板であるため、有機樹脂皮膜にMCAを配合するだけでは、得られる有機複合表面処理鋼板はプレス成形に必要な摺動性を確保することができない。そのため、プレス成形時の摺動性をさらに改善するために、MCAに加えてポリオレフィンワックス（例、ポリエチレンワックス）も有機樹脂皮膜に配合する。

【0038】有機樹脂皮膜中におけるポリオレフィンワックスの配合量は、乾燥皮膜重量に対して1～20重量%、好ましくは1～15重量%の範囲内である。1重量%未満では、MCAとの併用でも表面処理鋼板のプレス成形が困難であり、20重量%を超えると、電着塗膜の密着性が低下するようになる。

【0039】(7) シリカ  
前述したように、亜鉛系めっき鋼板を基材とする本発明の表面処理鋼板の耐低温チッピング性を改善するために、クロメート皮膜とその上の有機樹脂皮膜の一方または両方にシリカを含有させる。シリカの含有により得られる有機複合表面処理鋼板の耐低温チッピング性が著しく改善されるメカニズムは必ずしも明らかではないが、シリカ粒子が存在することによって何らかの衝撃エネルギーの分散・吸収が起こるからではないかと考えられる。

【0040】①クロメート皮膜中のシリカ  
クロメート皮膜中に配合するシリカとしては、シリカゾル（水性コロイダルシリカ）とヒュームドシリカ（気相コロイダルシリカ）のいずれでもよい。使用するシリカは粒子の平均一次粒径が5～50 $\mu\text{m}$ のものが好ましい。

【0041】クロメート皮膜にシリカを配合する場合、皮膜中のシリカ含有量が $\text{SiO}_2/\text{Cr}$ 重量比で0.05～4.0、

好ましくは0.1～3.0となる量とする。この比が0.05未満では、耐低温チッピング性の改善効果が十分でなく、一方4.0を超えると、クロメート皮膜の絶縁性が大きくなって、スポット溶接性が低下する（溶接時のチップ損傷や通電不能が起こり易くなる）。

【0042】②有機樹脂皮膜中のシリカ  
有機樹脂皮膜中にシリカを配合する場合には、シリカゾル、ヒュームドシリカのいずれも適用できるが、特に溶接性、耐食性に優れたシリカゾルを使用する方が好ましい。好ましいシリカゾルは、シリカ粒子の平均一次粒径が2～20 $\mu\text{m}$ の範囲内のものである。有機樹脂皮膜にシリカを配合する場合、乾燥皮膜中のシリカ( $\text{SiO}_2$ )含有量が5～40重量%、好ましくは5～30重量%の量となるように含有させる。この量が5重量%未満では、所望の耐低温チッピング性改善効果が得られず、一方40重量%を超えると、上記と同様にスポット溶接性の低下を招く。

【0043】(8) シランカップリング剤  
先に述べたように、クロメート皮膜と有機樹脂皮膜の一方または両方に、任意添加成分としてシランカップリング剤を配合することができる。シランカップリング剤を配合すると、皮膜中のシリカ粒子の皮膜成分との密着性が高まる結果、めっき／クロメート／有機樹脂の各皮膜間の密着性や電着塗膜との密着性が向上するので、耐低温チッピング性の改善に一層の好結果が得られる。従って、クロメート皮膜および／または有機樹脂皮膜にシリカを含有させた場合には、併せてシランカップリング剤を配合してもよい。

【0044】シランカップリング剤の配合量は、クロメート皮膜または有機樹脂皮膜中に含有させたシリカの重量に対して $1 \times 10^{-5}$ 倍以上とすることが好ましい。シランカップリング剤の種類は、既存のものから適宜選択すればよい。

【0045】

【実施例】次に実施例により本発明を例示する。実施例中、%は特に指定のない限り重量%である。

【0046】実施例1

両面とも $R_a = 0.14 \mu\text{m}$ および $R_a = 0.8 \mu\text{m}$ の2種類の冷延鋼板（板厚0.8mm）に対して、両面にZn-13%Ni合金電気めっき（硫酸塩浴）を施した。このめっき皮膜の目付け量は片面当たり30 g/ $\text{m}^2$ であった。

【0047】両面のめっき皮膜上に、 $\text{SiO}_2/\text{Cr} = 1$ の重量比で気相シリカ（平均一次粒径15 $\mu\text{m}$ ）を含有する塗布型クロメート液を、金属Cr換算で60 mg/ $\text{m}^2$ のクロメート皮膜が形成されるようにバーコートで塗布し、板温度が150℃となるように60秒間加熱して、クロメート皮膜を形成した。

【0048】このクロメート皮膜上に、ウレタン変性エポキシ樹脂を主成分とし、架橋剤としてブロックイソシアネートを含有する塗布液をバーコートで膜厚を変化させて塗布し、板温度が150℃となるように60秒間加熱し

て塗膜を乾燥させて樹脂を架橋させ、有機複合表面処理鋼板を得た。使用した塗布液には、上記樹脂と架橋剤以外に、不揮発分合計重量に対して4%のMCAまたは20%の親水性ポリアミド樹脂のいずれかと、10%のポリエチレンワックスを配合し、使用前に十分に攪拌して分散させた。

【0049】得られた各有機複合表面処理鋼板のカチオン電着塗装性を次のようにして試験した。各試験鋼板から150 mm×70 mmの試験片を切り出し、その片面の半分(75 mm×70 mm)だけを600番の研磨紙で研磨して、樹脂皮膜とクロメート皮膜を取り除き、めっき面を露出させた。次いで、この面の全体に、塗装下地としてリン酸亜鉛処理を施した後、市販のカチオン電着塗料を使用して、研磨部に膜厚18 $\mu$ mの電着塗膜が形成される条件でカチオン電着塗装を行い、研磨部に18 $\mu$ m厚の電着塗膜が形成された時の非研磨部の電着塗膜の厚みを測定した。研磨部と非研磨部とで電着塗膜の厚みの差が小さいほど、電着塗装性は良好であると評価される。

【0050】試験結果を有機樹脂皮膜厚と非研磨部の電着膜厚との関係として図2に示す。この図からわかるように、特公平3-32638号に提案されている、親水性ポリアミド樹脂を有機樹脂皮膜中に含有させた表面処理鋼板を電着塗装した場合には、研磨部と非研磨部との電着膜厚差が大きく、この電着膜厚差は、有機樹脂皮膜の膜厚が大きいほど大きくなった。従って、研磨部に相当するプレス疵等の手入れ部では電着塗膜が薄くなり、電着塗装後に外観ムラが発生することになる。

【0051】これに対し、本発明により有機樹脂皮膜中にMCAを含有させると、有機樹脂皮膜の膜厚に関係なく、常に非研磨部でも研磨部と同じ厚みで電着塗装でき、電着塗装性に優れていた。これは、プレス疵の手入れ部などがあっても電着塗装後に外観ムラを生じることがなくなることを意味する。

【0052】なお、基材鋼板のRaの違いは電着塗装性には影響せず、使用した基材鋼板のRaが0.14 $\mu$ mと0.8 $\mu$ mのいずれであっても、ほぼ同じ結果が得られた。図2に示したのは、Raが0.14 $\mu$ mの場合である。

【0053】さらに、MCAを含有する有機樹脂皮膜の膜厚が0.5 $\mu$ mである試験鋼板について、上記電着塗装後に市販の自動車用塗料を用いて中塗り塗装(膜厚35 $\mu$ m)および上塗り塗装(膜厚35 $\mu$ m)を施し、非研磨部の塗装鮮映性を携帯用鮮明度光沢度計(PGD IV型)により測定した。その結果、Ra=0.14 $\mu$ mの鋼板を基材とした場合のPGD値は0.9であったのに対し、Ra=0.8 $\mu$ mの鋼板を基材とした場合のPGD値は0.7であった。明らかに、Raの小さい鋼板を基材とすると、塗装後の鮮映性は著しく向上した。

【0054】実施例2

Ra=0.14 $\mu$ mの冷延鋼板を基材として、実施例1と同様に有機複合表面処理鋼板を作製した。ただし、有機樹脂皮膜にはMCAを種々の割合で含有させ、その膜厚は1.0 $\mu$ mと一定にした。得られた有機複合表面処理鋼板の電着塗装性を実施例1と同様に試験した結果を、有機樹脂皮膜中のMCA含有量(塗布液の不揮発分合計量に対するMCA添加量)に対する非研磨部での電着膜厚の関係として図3に示す。

【0055】図3に示した結果から、有機樹脂皮膜中にMCAを0.1%以上の量で含有させると、研磨部と同じ膜厚で電着塗装することが可能となり、優れた電着塗装性を発揮できるようになることが判明した。

【0056】実施例3

両面ともRa=0.14 $\mu$ mの冷延鋼板(板厚0.7 mm)を基材とし、実施例1と同様に有機複合表面処理鋼板を作製した。使用した基材鋼板は、TS=300 N/mm<sup>2</sup>、YP=130 N/mm<sup>2</sup>、El=47%の引張特性を有していた。Zn-13%Ni合金めっき皮膜の目付け量は、片面当たり20 g/m<sup>2</sup>とし、その上にSiO<sub>2</sub>/Cr=1の重量比でシリカを含有するクロメート皮膜を金属Cr換算で50 mg/m<sup>2</sup>の付着量となるように形成した。最上層の有機樹脂皮膜層は、MCAおよびポリエチレンワックスの含有量(塗布液中の不揮発分合計量に対する添加量)を変化させて形成した。

【0057】得られた有機複合表面処理鋼板のプレス成形性を、絞り比2.0の円筒絞り試験による割れ発生の有無により評価した。また、電着塗膜の二次密着性を評価するために、各表面処理鋼板の試験片(未研磨)を、リン酸亜鉛処理後、母材のZn-13%Ni合金めっき鋼板に対して膜厚20 $\mu$ mの電着塗膜が形成される条件でカチオン電着塗装を行った。この電着塗装試験片を50℃の温水中に240時間浸漬した後、ごぼん目試験(1 mm間隔×100マス、セロファンテープ剥離)に付し、塗膜残存率により二次密着性を評価した。

【0058】試験結果を有機樹脂皮膜中のMCAおよびワックスの含有量とともに次の表1に示す。この試験結果からわかるように、本発明に従って有機樹脂皮膜がMCA0.1%以上とポリエチレンワックス1%以上の両者を含有している場合には、割れのない良好なプレス成形が可能であったが、これら添加成分の少なくとも一方が欠けるとプレス成形時に割れが発生した。即ち、ブライト鋼板を基材とする場合には、有機樹脂皮膜がMCAとワックスの両者を含有する必要があることがわかる。ただし、ワックスの含有量が20%の上限を超えると、プレス成形性は確保されるものの、電着塗膜の密着性が低下した。

【0059】

【表1】

1 1

1 2

試験 No.	MCA 含有量	ワックス 含有量	プレス 成形性	電着塗膜 二次密着性	区 分
1	0%	0%	割れ	100%	比較例
2	0.1%	0%	割れ	100%	比較例
3	0%	1%	割れ	100%	比較例
4	0.1%	1%	良好	100%	本発明
5	0.1%	20%	良好	100%	本発明
6	0.1%	30%	良好	90%	比較例

## 【0060】実施例4

両面とも $Ra=0.18\mu m$ の冷延鋼板(板厚0.8 mm)に対して、両面に表2に示す目付け量のZn-13%Ni合金めっきまたはZn-9%Fe合金めっきを、硫酸塩浴による電気めっき法で施した。その後、実施例1と同様の方法で、めっき皮膜上に塗布型クロメート皮膜とエポキシ系樹脂を主成分とする有機樹脂皮膜とを形成して、有機複合表面処理鋼板を作製した。クロメート皮膜の付着量(Cr換算)と樹脂皮膜の膜厚は、表2に示すように変化させた。

【0061】使用したクロメート液には、場合によりコロイダルシリカ(平均一次粒径 $10m\mu$ )とシランカップリング剤(γ-クリシドキシプロピルトリメトキシシラン)の一方または両方を添加した。シリカの添加量( $SiO_2$ /Cr重量比)とシランカップリング剤の添加量(対 $SiO_2$ 重量比)を表2に示す。

【0062】有機樹脂皮膜の形成に使用した塗布液は、ビスフェノールA系エポキシ樹脂と架橋剤のブロックイソシアネートを含む塗料に、不揮発分合計量に対して5%のMCAと3%のポリエチレンワックスとを分散させたものであり、さらに場合によりシリカゾル(平均一次粒径 $10m\mu$ )と上と同じシランカップリング剤の一方または両方を配合した。この塗布液への $SiO_2$ 添加量(不揮発分に対する%)とシランカップリング剤の添加量(対 $SiO_2$ 重量比)は表2に示す通りである。

【0063】得られた有機複合表面処理鋼板の耐低温チップング性、Cr溶出量、耐外面錆性、およびスポット溶\*

\*接性を次の試験方法により調査した。試験結果も表2に合せて示す。

【0064】(耐低温チップング性)試験片に電着塗装 $30\mu m$ 、自動車塗り塗料 $40\mu m$ の2コート2ベークの塗装を施した後、 $-20^\circ C$ に冷却してグラベロテスターで小石の衝撃を与え、この箇所をセロファンテープで剥離した。剥離後のめっき/鋼板界面での剥離径を測定した。

20 【0065】(Cr溶出量)試験片を $40^\circ C$ のアルカリ脱脂液(日本パーカライジング社製FC4410)中に2分間浸漬して脱脂を行い、その前後における試験片のCr付着量を蛍光X線により測定し、Cr溶出量を算出した。

【0066】(耐外面錆性)試験片に電着塗装 $30\mu m$ 、自動車塗り塗料 $40\mu m$ の2コート2ベークの塗装を施した後、カッターナイフで基材鋼板に達する深さのクロスカット疵を入れ、週2回の塩水散布を含む屋外暴露を3カ月実施した後、カット部からの赤錆発生の有無を目視で判定した。

30 【0067】(スポット溶接性)同じ有機複合表面処理鋼板の試験片2枚を重ねあわせ、先端径6mmのCu-Cr合金製電極チップを備えた交流シングルスポット溶接器(50 Hz)を用いて、溶接電流10 kA、スクイズ時間20サイクル、通電時間12サイクル、保持5サイクル、加圧力200 Kgの条件でスポット溶接連続打点試験を行った。剪断引張りで溶接剥がれが生じた打点数をもって、スポット溶接性を評価した。

【0068】

【表2】



13

14

区分	試験No	亜鉛系めっき		クロメート皮膜			エポキシ系樹脂皮膜			耐低温 チップリング性 (めっき剥離径) (mm)	Cr溶出量 (mg/m <sup>2</sup> )	耐外面錆性	スポット 溶接性 (打点数)
		めっき種	付着量 (g/m <sup>2</sup> )	Cr付着量 (mg/m <sup>2</sup> )	SiO <sub>2</sub> /Cr 重量比	シランカップ リング剤量 <sup>1)</sup>	膜厚 (μm)	SiO <sub>2</sub> 量 (wt%)	シランカップ リング剤量 <sup>1)</sup>				
本発明例	1	Zn-13%Ni	10	40	0.4	1×10 <sup>-4</sup>	0.5	5	0	0.2	0.2	赤錆発生なし	>5000
	2		20	20	0.6	1×10 <sup>-3</sup>	0.5	8	1×10 <sup>-4</sup>	0.3	0.6	赤錆発生なし	>5000
	3		20	190	0.07	0	0.5	12	0	0.3	2.0	赤錆発生なし	>5000
	4		30	60	3.8	1×10 <sup>-5</sup>	0.4	18	1×10 <sup>-5</sup>	0	1.0	赤錆発生なし	4100
	5		30	50	0.9	0	1.9	20	0	0	0.5	赤錆発生なし	3500
	6		20	30	1.2	0	0.8	35	0	0.2	0.3	赤錆発生なし	3500
	7		30	70	0	0	1.8	25	0	0.2	0.1	赤錆発生なし	3500
比較例	8	Zn-9%Fe	35	30	0.6	0	0.6	10	0	0	0.8	赤錆発生なし	>5000
	9		45	60	0.6	0	0.5	0	0	0.3	0.6	赤錆発生なし	>5000
	10	Zn-13%Ni	30	0*	0	0	0*	0	0	3.6	0	赤錆発生なし	>5000
	11		0*	50	0.5	1×10 <sup>-5</sup>	0.7	10	1×10 <sup>-5</sup>	0.1	0.1	赤錆発生あり	>5000
	12		30	10*	0.5	1×10 <sup>-3</sup>	0.7	10	1×10 <sup>-4</sup>	2.1	0.2	赤錆発生なし	>5000
	13		30	250*	0.5	1×10 <sup>-3</sup>	0.7	10	1×10 <sup>-4</sup>	0	4.8	赤錆発生なし	4200
	14		30	70	5.0*	1×10 <sup>-5</sup>	0.4	15	1×10 <sup>-5</sup>	0.1	0.1	赤錆発生なし	2000
	15		30	50	0.5	0	0.01*	15	0	0.9	4.7	赤錆発生なし	>5000
	16		30	50	0.5	0	3.0*	15	0	0.1	0.1	赤錆発生なし	0(不能)
	17		20	50	0*	0	1.0	0*	0	3.2	0.1	赤錆発生なし	>5000
	18		20	50	0.5	0	1.0	50*	0	0.1	0.1	赤錆発生なし	2500

(注) \* 本発明の範囲外； 1) シランカップリング剤量は (シランカップリング剤D/(SiO<sub>2</sub>)) の重量比。

【0069】表2から分かるように、本発明による有機複合表面処理鋼板は、試験したいずれの性能にも優れていた。これに対し、比較例には、クロメート皮膜の付着量または有機樹脂皮膜の膜厚が本発明の範囲外であるか、クロメート皮膜と有機樹脂皮膜の両方がシリカを含有しないか、あるいはそのシリカの含有量が本発明の範囲外である例を示した。これらの比較例では、耐低温チ\*50

\* ッピング性、Cr溶出量、耐外面錆性、スポット溶接性の少なくとも一つの性能が劣り、全ての性能を満たす有機複合表面処理鋼板を得ることができなかった。なお、本実施例で作製した有機複合表面処理鋼板の電着塗装性はいずれも良好であった。

【0070】

【発明の効果】以上詳述したように、本発明の有機複合



表面処理鋼板が得られる。従って、本発明の表面処理鋼板から自動車車体を製造すると、自動車の外観と耐久性の著しい向上が期待でき、産業上極めて有用な効果がもたらされる。

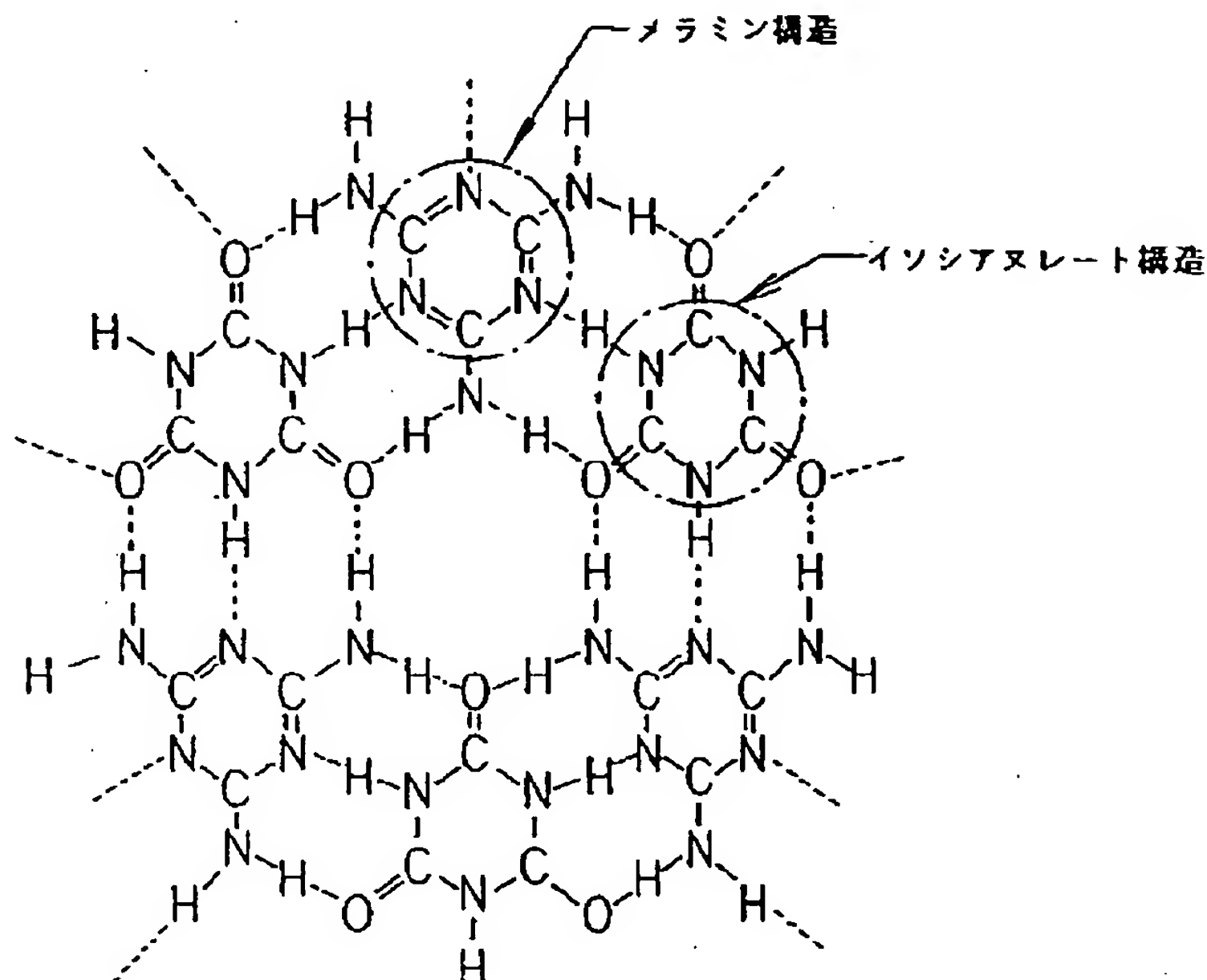
【図1】MCA（メラミンシアヌル酸付加体）の化学構造を示す。

を、有機樹脂皮膜厚と非研磨部の電着膜厚との関係として示すグラフである。

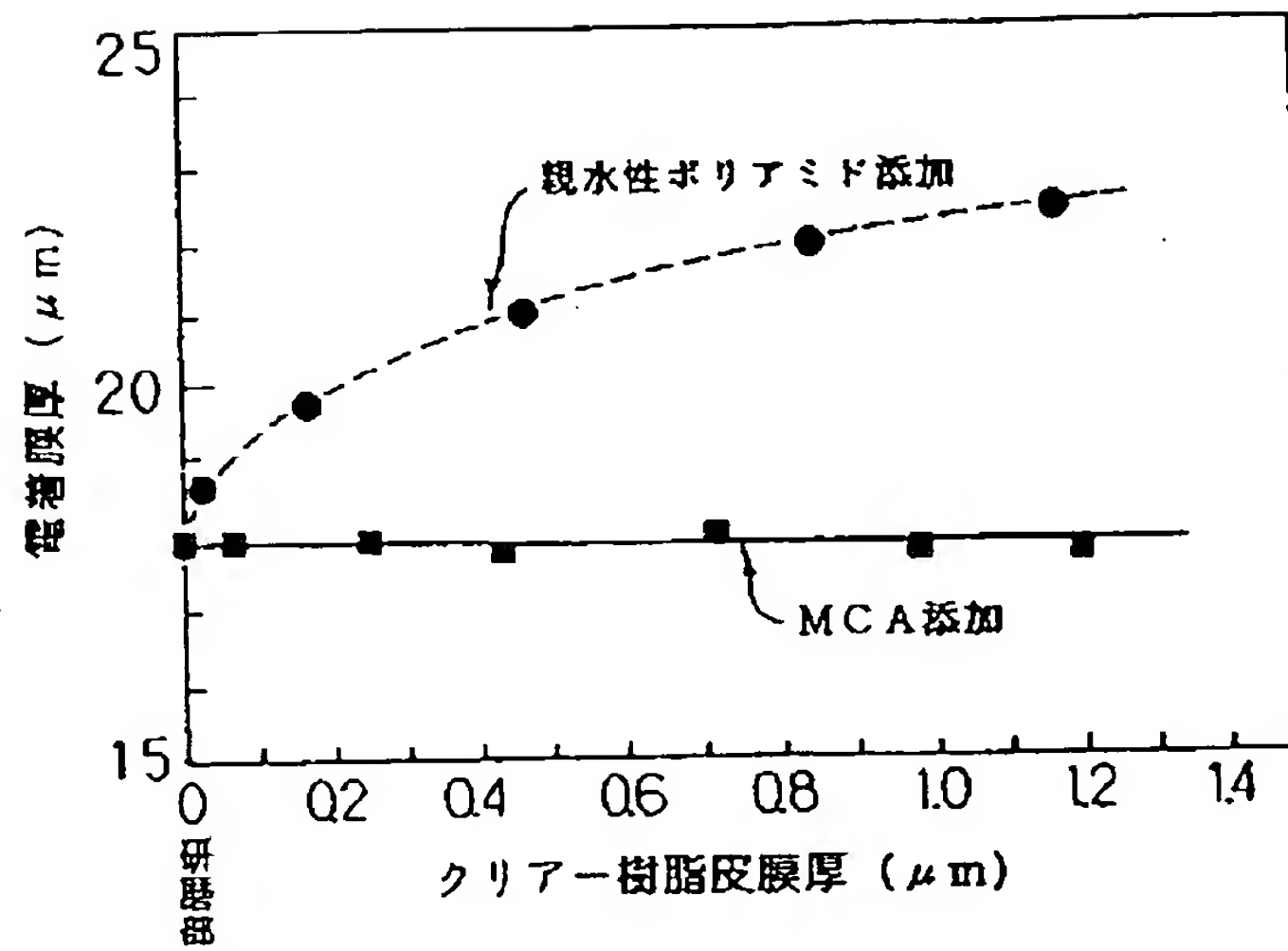
【図3】MCAを含有する有機樹脂皮膜を有する有機複合表面処理鋼板の電着塗装性を、有機樹脂皮膜中のMCA含有量と非研磨部の電着膜厚との関係として示すグラフである。

【0071】しかも、架橋エポキシ系樹脂からなる有機樹脂皮膜中に存在するMCAとこの樹脂皮膜または下層のクロメート皮膜の少なくとも一方に含有させるシリカの作用によって、優れた耐食性やスポット溶接性を保持したまま、カチオン電着塗装性と耐低温チップング性も著しく改善され、自動車外装用鋼板の内外両面に要求される性能をすべて満たすことができる自動車用有機複合

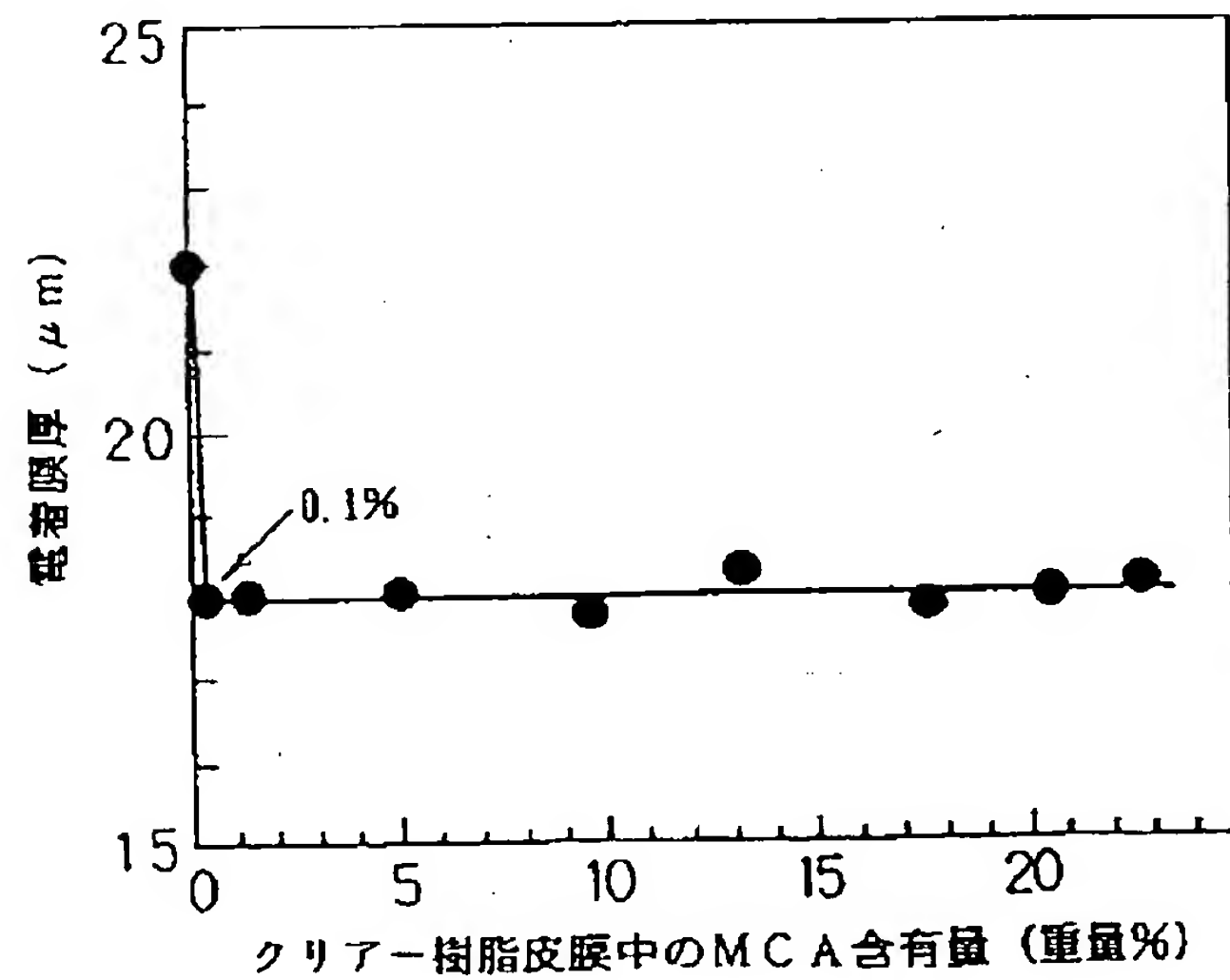
【図 1】



【図2】



【図3】



フロントページの続き

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技術表示箇所